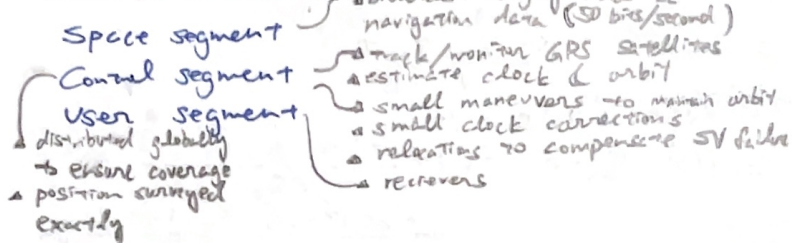


Ch1 Basics

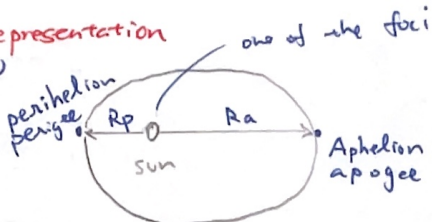
GPS Architecture



Satellite position representation

Kepler's three law

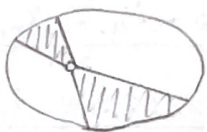
- The law of orbit: $R_a = a(1+e)$, $R_p = a(1-e)$



e = eccentricity of the ellipse

The law of areas

$$\frac{A_0}{t_1 - t_0} = \frac{A_1}{t_2 - t_1}$$



area velocity = const.

The law of period

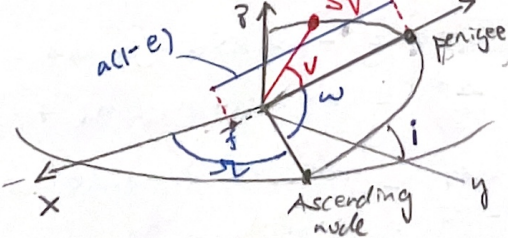
$$\frac{R_0^3}{T_0^2} = \frac{R_1^3}{T_1^2}$$

Semi-major axis orbital period



Keplerian Elements

- orbit shape: a semimajor axis, e eccentricity
- orbit orientation: i inclination, Ω right ascension of ascending node, ω angle of perigee
- Satellite angular position: v true anomaly



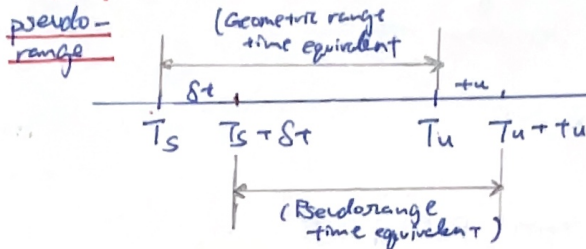
Coordinate Transformation

- Keplerian parameters
- Peri-focal coordinates
- Earth centered inertial
- Earth centered earth-fixed (World Geodetic System WGS-84)

Factors that affect satellite orbit/clock

- perturbation forces:
 - non sphericity of earth's gravitational potential
 - 3rd body effects
 - solar radiation pressure
- relativity effects:
 - less gravity \rightarrow time faster
 - faster speed \rightarrow time slower

TOA & GNSS measurement



$$P = c[(T_u + \delta t) - (T_s + \delta t)] + \sum \delta$$

$$= \frac{c(T_u - T_s)}{\text{Geometric Range}} + \frac{c(\delta t - \delta t)}{\text{Clock offset from system time}} + \sum \delta$$

$T_u + \delta t$, $T_s + \delta t$ are obtained from

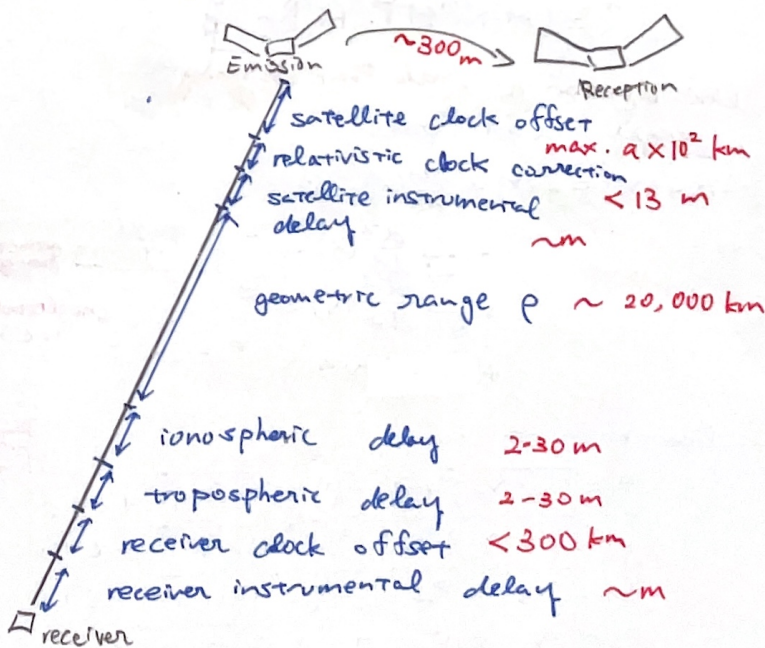
- Ranging codes & non-synchronized clock

Carrier phase

$$P = \lambda \cdot \Delta \phi = \lambda (\underbrace{\phi_r(T_2)}_{\text{phase of signal reception}} - \underbrace{\phi_s(T_1)}_{\text{phase of signal transmission}})$$

- much more precise
- yet w/ ambiguity on integer of existing wavelengths

pseudo-range error source



Least Squares

$x \in \mathbb{R}^n$ (tracking state)
 $y \in \mathbb{R}^m$ (observation state)

$$\begin{cases} y = Hx + n \\ \hat{x} = \underset{x}{\operatorname{argmax}} P(y|x) \end{cases}$$

$n \sim N(0, \Sigma)$

$$\hat{x} = \underset{x}{\operatorname{argmax}} \frac{1}{(2\pi\sigma)^{N/2}} e^{-\frac{1}{2\sigma^2} \|y - Hx\|^2}$$

$$= \underset{x}{\operatorname{argmin}} \|y - Hx\|^2$$

\therefore we set $\frac{d}{d\hat{x}} \|y - H\hat{x}\|^2 = 2H^T H\hat{x} - 2H^T y$

$\therefore \hat{x} = (H^T H)^{-1} H^T y$

Δ weighted version

$$\hat{x} = \underset{x}{\operatorname{argmax}} \frac{1}{(2\pi)^{\frac{N}{2}} |R_n|^{\frac{1}{2}}} e^{-\frac{1}{2} (y - Hx)^T R_n^{-1} (y - Hx)}$$

$$= \underset{x}{\operatorname{argmin}} (y - Hx)^T R_n^{-1} (y - Hx)$$

$\therefore \hat{x} = (H^T R_n^{-1} H)^{-1} H^T R_n^{-1} y$

Linearization (Single Point Positioning)

Δ recall Taylor Series

$$f(x + \Delta x) = f(x) + \frac{df}{dx}(x) \cdot \Delta x + \frac{1}{2!} \frac{d^2 f}{dx^2}(x) \Delta x^2 + \frac{1}{3!} \frac{d^3 f}{dx^3}(x) \Delta x^3 + \mathcal{O}(\Delta x^4)$$

*recall pseudo-range $p = c(t_u - t_s)$ geometry change
 $+ c(t_u - t_s) + \epsilon \delta$ (neglect here)
 $= r + c(t_u - t_s)$
 region offset \rightarrow satellite known here (broadcast)*

Δ linearization \rightarrow solve

$$\begin{matrix} p_1 = \sqrt{(x_1 - x_u)^2 + (y_1 - y_u)^2 + (z_1 - z_u)^2} + c t_u \\ p_2 = \sqrt{(x_2 - x_u)^2 + (y_2 - y_u)^2 + (z_2 - z_u)^2} + c t_u \\ p_3 = \sqrt{(x_3 - x_u)^2 + (y_3 - y_u)^2 + (z_3 - z_u)^2} + c t_u \\ p_4 = \sqrt{(x_4 - x_u)^2 + (y_4 - y_u)^2 + (z_4 - z_u)^2} + c t_u \end{matrix}$$

known known \leftarrow
 Δ unknowns

$$\Delta \rightarrow p_j = \sqrt{(x_j - x_u)^2 + (y_j - y_u)^2 + (z_j - z_u)^2} + c t_u = f(x_u, y_u, z_u, t_u)$$

assume a known, approximate position location $(\hat{x}_u, \hat{y}_u, \hat{z}_u)$ & \hat{t}_u (time bias)

$$\hat{p}_j = \sqrt{(x_j - \hat{x}_u)^2 + (y_j - \hat{y}_u)^2 + (z_j - \hat{z}_u)^2} + c \hat{t}_u = f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u) \quad \text{--- } \textcircled{*}$$

$\Delta \rightarrow x_u = \hat{x}_u + \Delta x_u \quad z_u = \hat{z}_u + \Delta z_u$
 $y_u = \hat{y}_u + \Delta y_u \quad t_u = \hat{t}_u + \Delta t_u$

$$\therefore f(x_u, y_u, z_u, t_u) = f(\hat{x}_u + \Delta x_u, \hat{y}_u + \Delta y_u, \hat{z}_u + \Delta z_u, \hat{t}_u + \Delta t_u)$$

\therefore TS of $f(x_u, y_u, z_u, t_u)$:

$$\begin{aligned} f(x_u, y_u, z_u, t_u) &= f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u) + \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial x_u} \Delta x_u \\ &+ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial y_u} \Delta y_u \\ &+ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial z_u} \Delta z_u \\ &+ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial t_u} \Delta t_u \\ &+ \mathcal{O}(\Delta^2) \quad \text{--- } \textcircled{*} \end{aligned}$$

(from above)

$$\begin{aligned} \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial x_u} &= - \frac{x_j - \hat{x}_u}{\hat{r}_j} \\ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial y_u} &= - \frac{y_j - \hat{y}_u}{\hat{r}_j} \\ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial z_u} &= - \frac{z_j - \hat{z}_u}{\hat{r}_j} \\ \frac{\partial f(\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u)}{\partial t_u} &= c \end{aligned}$$

$$\hat{r}_j = \sqrt{(x_j - \hat{x}_u)^2 + (y_j - \hat{y}_u)^2 + (z_j - \hat{z}_u)^2}$$

Δ put $\textcircled{*}$ & $\textcircled{+}$ into $\textcircled{*}$

we get

$$p_j = \hat{p}_j - \frac{a_{xj}}{\hat{r}_j} \Delta x_u - \frac{a_{yj}}{\hat{r}_j} \Delta y_u - \frac{a_{zj}}{\hat{r}_j} \Delta z_u + c \Delta t_u$$

$$\begin{aligned} \Rightarrow p_j - \hat{p}_j &= -a_{xj} \Delta x_u - a_{yj} \Delta y_u - a_{zj} \Delta z_u + c \Delta t_u \\ \Rightarrow \Delta p_j &= a_{xj} \Delta x_u + a_{yj} \Delta y_u + a_{zj} \Delta z_u - c \Delta t_u \\ \Rightarrow \Delta p_1 &= a_{x1} \Delta x_u + a_{y1} \Delta y_u + a_{z1} \Delta z_u - c \Delta t_u \\ \Delta p_2 &= a_{x2} \Delta x_u + a_{y2} \Delta y_u + a_{z2} \Delta z_u - c \Delta t_u \\ \Delta p_3 &= a_{x3} \Delta x_u + a_{y3} \Delta y_u + a_{z3} \Delta z_u - c \Delta t_u \\ \Delta p_4 &= a_{x4} \Delta x_u + a_{y4} \Delta y_u + a_{z4} \Delta z_u - c \Delta t_u \end{aligned}$$

$$\Rightarrow \Delta p = \begin{bmatrix} \Delta p_1 \\ \Delta p_2 \\ \Delta p_3 \\ \Delta p_4 \end{bmatrix} = H \begin{bmatrix} \Delta x_u \\ \Delta y_u \\ \Delta z_u \\ \Delta t_u \end{bmatrix} \quad H = \begin{bmatrix} a_{x1} & a_{y1} & a_{z1} & -c \\ a_{x2} & a_{y2} & a_{z2} & -c \\ a_{x3} & a_{y3} & a_{z3} & -c \\ a_{x4} & a_{y4} & a_{z4} & -c \end{bmatrix}$$

$\Rightarrow \Delta p = H \Delta x \rightarrow$ could be > 4 over-determined
 get Δx (can use least-square)
 get $(x_u, y_u, z_u, t_u) = (\hat{x}_u, \hat{y}_u, \hat{z}_u, \hat{t}_u) + \Delta x$

Dilution of Precision (DOP)



$$\begin{aligned}
 \text{PDOP/GDOP} &= \sqrt{D_{11} + D_{22} + D_{33} + D_{44}} \\
 \text{HDOP} &= \sqrt{D_{11} + D_{22}} \\
 \text{VDOP} &= \sqrt{D_{33}} \\
 \text{TDOP} &= \sqrt{D_{44}} / c
 \end{aligned}$$

$$H \Delta x = \Delta p$$

$$H = \begin{bmatrix} a_{x1} & a_{y1} & a_{z1} & 1 \\ a_{x2} & a_{y2} & a_{z2} & 1 \\ \vdots & \vdots & \vdots & \vdots \\ a_{xn} & a_{yn} & a_{zn} & 1 \end{bmatrix}$$

$$\begin{aligned}
 \Delta x &= (H^T H)^{-1} H^T \Delta p \\
 \text{cov}(\Delta x) &= (H^T H)^{-1} \sigma_{\text{USER}}^2
 \end{aligned}$$

user equivalent range error

$$(H^T H)^{-1} = \begin{bmatrix} D_{11} & D_{12} & D_{13} & D_{14} \\ D_{21} & D_{22} & D_{23} & D_{24} \\ D_{31} & D_{32} & D_{33} & D_{34} \\ D_{41} & D_{42} & D_{43} & D_{44} \end{bmatrix}$$

- better geometry, less DOP
- VDOP > HDOP, no variation vertically
- precise → concentrated data accurate → ground-truth-closed data

SV clock correction

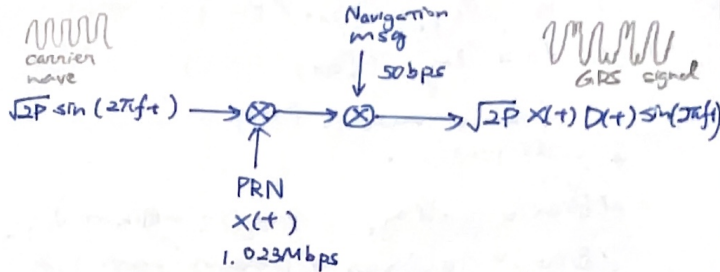
- ▷ satellite clock offset
 - monitored by ground station network
 - rebroadcasted to receiver
- ▷ clock correction model
 - thru polynomial
 - polynomial coefficients a_0, a_1, a_2
 - prediction model (hours to days)
 - reference by T_{oc} → operation center

Ch3 GPS/GNSS signal

Signal Structure

$$\text{signal} = \text{carrier wave} + \text{PRN code}$$

ephemeris
satellite clock/correction
navigation msg
PRN code
Sat. Time of Arrival



- carrier wave @ 1575.42 MHz, L1, is modulated by
 - coarse/acquisition (C/A) code civilians
 - precision/secure (P/Y) code military

PRN (Pseudo Random Noise) Code

Δ for measurement of time of arrival (TOA)
Δ generation pattern: Gold Code

- Δ 1 second : 50 bit
- 1000 ms : 50 bit
- 20 ms : 1 bit
- 20 ms : 20 repetition of C/A
- 1 ms : 1 repetition of C/A
- 1 repetition of C/A : 1023 $\frac{1}{0}$

Δ C/A : 1.023 M cps
P/Y : 10.23 M cps

Signal @ L-band lower frequency gets easier to be affected by ionosphere

Auto-correlation

- ① Satellite transmits code-phase with timestamp $T_S(n)$
- ② Receiver receives code-phase with timestamp $T_R(n)$
n here stands for epoch n
- ③ on timeline of "Receiver", a replica code-phase is generated at $T_S(n)$ on timeline "receiver"
- ★ ④ conduct auto-correlation by shifting the replica code-phase to match received code-phase on timeline receiver
- ⑤ the shifted Δt is the inferred propagation time
- ⑥ pseudorange = $c \cdot \Delta t$
- ⑦ this pseudorange = $c [(T_u + t_u) - (T_s + \delta t)] + \epsilon$

Carrier Phase: resolve fractional difference / integer ambiguity (N)
could get accuracy of 1-2cm

Power of GPS

- Bel $B = \log_{10} (P_{out} / P_{in})$
- Decibel $dB = 10 \log_{10} (P_{out} / P_{in})$
- set reference value (P_{in})
1 milliwatt:

$dBm = 10 \log_{10} (\text{power in milliwatt}) / 1 \text{ milliwatt}$
 $dBW = 10 \log_{10} (\text{power in watt}) / 1 \text{ watt}$

Path Loss

- transmit power is 27W
 - received power reduced by 10^{16}
 - 130 dBm
 - 160 dBm
- Thermal Noise Power -110 dBm < WiFi BT Phones

Antenna Gain: ratio of $\frac{\text{entire sphere area}}{\text{spot area}}$

Ch4 Differential Positioning & Precise Positioning

Errors

$\delta t_p = \delta t_{atm} + \delta t_{\text{noise inter.}} \rightarrow \delta t_{\text{mp multi-path}} + \delta t_{\text{hw hardware}}$

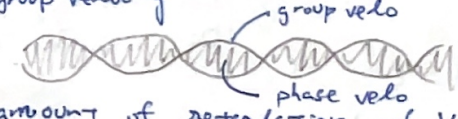
Satellite Clock Error

- offset of SV time to GPS time
- curve-fit to model the clock correction (polynomial coefficients in navmsg)
- not location-dependent for users

Ephemeris Error

- due to perturbation forces
- curve-fit to model the error
- location-dependent for users (increases with separation)
base station receiver

Ionosphere Delay

- 電離層
 - affects electromagnetic wave propagation
 - dispersive medium $15 \times 10^6 \text{ MHz}$
 - $f > f_c \approx 10^6 \text{ Hz}$ can travel thru
 - phase velocity will exceed group velocity
- 
- amount of retardation of V_{group} = advance of carrier phase w.r.t. free-space propagation
 - GPS: PRN & navmsg carrier phase delayed than ionospheric divergence
 - removed by dual receiver
 - depend on frequency f , elevation angle ϕ' (@iono. piercept), total electron content TEC
 - location-dependent for users (increases w/ separation)
base station receiver

Troposphere Delay

- 對流層
 - nondispersive, but with refraction
- | | |
|--|--------------------------|
| dry (hydrostatic) | wet (nonhydrostatic) |
| - 90% to delay | - lesser to delay |
| - predict accurately | - difficult to predict |
| - extends to 40km height | - extends to 10km height |
| - utilize troposphere model to predict | |

basically depends on weather

- location-dependent for users

Receiver Noise

- thermal noise jitter
- interference/jamming (malicious signal)

Multipath



- depends on environment
 - receiver location
 - satellite elevation angle
 - receiver signal processing
 - antenna gain pattern
 - signal characteristics
- improvements:
 - detect received signal pattern thru signal/noise density ratio to see reflection/refraction
 - signal processing: reduce early/late correlator
 - antenna: increase directivity

Hardware Bias

- Satellite Bias
 - signals and carrier frequency not totally synced.
- Receiver/Equipment Bias
 - signals are delayed in hardware

1. From above, usually (single point), dominant pseudorange error: "Ionospheric Delay"

→ could be removed w/ dual receiver

2. Spatially correlated:

- Ephemeris Errors
- Ionospheric Error
- Tropospheric Error
- multipath

Real-Time Kinematic (RTK)

- base receiver + rover receiver (22)
- base receiver process GPS signals
- rover receiver process GPS signals
- base station broadcast its measurement rover receiver
- rover receiver could then resolve some error like ionospheric errors
- harnesses both pseudo-range (code) & carrier phase

m → cm

typical algo.

1. KF
2. unknowns: X_{rover} , V_{rover} , ambg.
3. measurements: double differenced carrier phase, double differenced pseudo-range
 - a. EKF update
 - b. solve ambg. improve accuracy convergence time
4. Integer ambg. solution:

Precise Point Positioning (PPP)

- single receiver
- relies on precise satellite clock orbit products correction ↑ from global stations.
- cm-level.
- PPP performance > RTK

Ch5 Augmentation Systems

differential positioning (relative positioning)

- 2 receivers are close
- track difference between the 2
 - can be tracked more accurately
 - iono + tropo + clock + ephemeris errors are cancelled.
- $\Delta X = (P_1, t_1) - (P_2, t_2)$
 - ↳ know ΔX , know reference get rover.
- base station, with high-performance GPS receiver, could calculate error/correction & send correction to rover.

DGPS = reference station + data link + user receiver

- Local Area Differential GPS
- Wide Area Differential GPS

Ground Based Augmentation Systems (GBAS)

- pseudo-range corrections
- use/don't use
- Aviation
- DGPS

Satellite Based Augmentation Systems (SBAS)

- Aviation
- DGPS
- iono., clock, ephemeris.
- GEO
- monitored / not monitored
- use / don't use

- send corrections
- send integrity msgs.