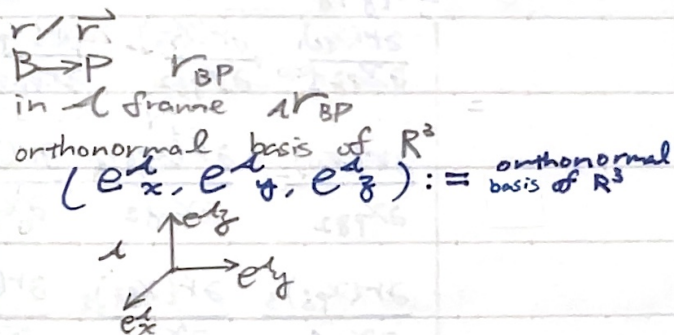


Robot Dynamics Fundamentals

vector



parameterization of ${}^{\mathcal{R}}r_{AB} = x e_x + y e_y + z e_z$

Cartesian coordinates

$$x_{PC} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$\Delta {}^{\mathcal{R}}r_{AB} = x e_x + y e_y + z e_z$$

Cylindrical coordinates

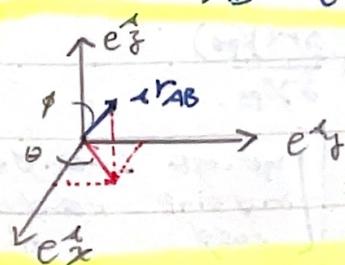
$$x_{P\zeta} = \begin{pmatrix} \rho \\ \theta \\ z \end{pmatrix}$$

$$\Delta {}^{\mathcal{R}}r_{AB} = \begin{pmatrix} \rho \cos \theta \\ \rho \sin \theta \\ z \end{pmatrix}$$

Spherical coordinates

$$x_{PS} = \begin{pmatrix} r \\ \theta \\ \phi \end{pmatrix}$$

$$\Delta {}^{\mathcal{R}}r_{AB} = \begin{pmatrix} r \sin \theta \cos \phi \\ r \sin \theta \sin \phi \\ r \cos \theta \end{pmatrix}$$



ex 1-1.

$${}^{\mathcal{R}}r_{AP} = {}^{\mathcal{R}}r_{AB} + {}^{\mathcal{R}}r_{BP}$$

$$\begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} + \begin{pmatrix} 0 \\ 1 \\ 1 \end{pmatrix}$$

get $\begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} : \begin{cases} x_{PC} = \\ x_{P\zeta} = \\ x_{PS} = \end{cases}$

$\begin{pmatrix} 0 \\ 1 \\ 1 \end{pmatrix} : \begin{cases} x_{PC} = \\ x_{P\zeta} = \\ x_{PS} = \end{cases}$

$\begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} : \begin{cases} x_{PC} = \\ x_{P\zeta} = \\ x_{PS} = \end{cases}$

$$\begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} x_{PC} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \rho \cos \theta \\ \rho \sin \theta \\ z \end{pmatrix} = \begin{pmatrix} r \sin \theta \cos \phi \\ r \sin \theta \sin \phi \\ r \cos \theta \end{pmatrix}$$

$$\therefore \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 \cos 0^\circ \\ 1 \sin 0^\circ \\ z \end{pmatrix} = \begin{pmatrix} 1 \sin 90^\circ \cos 0^\circ \\ 1 \sin 90^\circ \sin 0^\circ \\ 1 \cos 90^\circ \end{pmatrix}$$

$$x_{P\zeta} = \begin{pmatrix} 1 \\ 0^\circ \\ 0 \end{pmatrix}$$

$$x_{PS} = \begin{pmatrix} 1 \\ 0^\circ \\ 90^\circ \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ 1 \\ 1 \end{pmatrix} x_{PC} = \begin{pmatrix} 0 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} \rho \cos \theta \\ \rho \sin \theta \\ z \end{pmatrix} = \begin{pmatrix} r \sin \theta \cos \phi \\ r \sin \theta \sin \phi \\ r \cos \theta \end{pmatrix}$$

$$\therefore \begin{pmatrix} 0 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} 1 \cos 90^\circ \\ 1 \sin 90^\circ \\ z \end{pmatrix} = \begin{pmatrix} \sqrt{2} \sin 45^\circ \cos 90^\circ \\ \sqrt{2} \sin 45^\circ \sin 90^\circ \\ \sqrt{2} \cos 45^\circ \end{pmatrix}$$

$$x_{P\zeta} = \begin{pmatrix} 90^\circ \\ 1 \\ 0 \end{pmatrix}$$

$$x_{PS} = \begin{pmatrix} \sqrt{2} \\ 90^\circ \\ 45^\circ \end{pmatrix}$$

$$\begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} x_{PC} = \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} \sqrt{2} \cos 45^\circ \\ \sqrt{2} \sin 45^\circ \\ 1 \end{pmatrix} = \begin{pmatrix} \sqrt{2} \sin(\arctan \sqrt{2}) \cos 45^\circ \\ \sqrt{2} \sin(\arctan \sqrt{2}) \sin 45^\circ \\ \sqrt{2} \cos(\arctan \sqrt{2}) \end{pmatrix}$$

$$x_{P\zeta} = \begin{pmatrix} \sqrt{2} \\ 45^\circ \\ 1 \end{pmatrix}$$

$$x_{PS} = \begin{pmatrix} \sqrt{2} \\ 45^\circ \\ \arctan \sqrt{2} \end{pmatrix}$$

vector derivatives (linear velocity)

$r = r(\chi)$ vector being represented by specific parameterization

$$\dot{r} = \dot{r}(\chi) \dot{\chi}$$

$$\Rightarrow \dot{r} = \frac{\partial r}{\partial \chi} \dot{\chi}$$

$E_P(\chi)$

$$\dot{r} = E_P(\chi) \dot{\chi}$$

$$E_P(\chi)^{-1} \dot{r} = \dot{\chi}$$

$r = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$ Cartesian coordinates

$$x_{PC} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$\therefore E_{PC}(x_{PC}) = E_{PC}^{-1}(x_{PC}) = I$$

Cylindrical coordinates

$$r = \begin{pmatrix} \rho \cos \theta \\ \rho \sin \theta \\ z \end{pmatrix}$$

matrix calculus

vector-by-vector

$$\frac{\partial y}{\partial x} (x, y \in \mathbb{R}^n)$$

$$\frac{\partial y}{\partial x} = \begin{bmatrix} \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_n} \\ \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_n} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial y_n}{\partial x_1} & \dots & \dots & \frac{\partial y_n}{\partial x_n} \end{bmatrix}$$

$$r(x_{ps}) = [\rho \cos \theta \ \rho \sin \theta \ z]^T$$

$$x_{ps} = [\rho \ \theta \ z]^T$$

calculus revision

e.g. $\nabla f = \frac{\partial f}{\partial x} = \left[\frac{\partial f}{\partial x_1} \quad \frac{\partial f}{\partial x_2} \quad \frac{\partial f}{\partial x_3} \right]$ (gradient)

\mathbb{R}^3

vector by scalar $y = [y_1, y_2, \dots, y_m]^T$, x

$$\frac{\partial y}{\partial x} = \begin{bmatrix} \frac{\partial y_1}{\partial x} \\ \frac{\partial y_2}{\partial x} \\ \vdots \\ \frac{\partial y_m}{\partial x} \end{bmatrix}$$

e.g. position
↓
velocity

scalar by vector y , $x = [x_1, x_2, \dots, x_n]^T$

$$\frac{\partial y}{\partial x} = \left[\frac{\partial y}{\partial x_1}, \frac{\partial y}{\partial x_2}, \dots, \frac{\partial y}{\partial x_n} \right]$$
 e.g. gradient

$$\nabla f = \begin{bmatrix} \frac{\partial f}{\partial x_1} \\ \vdots \\ \frac{\partial f}{\partial x_n} \end{bmatrix} = \left(\frac{\partial f}{\partial x} \right)^T$$

vector by vector $y = [y_1, y_2, \dots, y_m]^T$
 $x = [x_1, x_2, \dots, x_n]^T$

$$\frac{\partial y}{\partial x} = \begin{bmatrix} \frac{\partial y_1}{\partial x_1} & \frac{\partial y_1}{\partial x_2} & \dots & \frac{\partial y_1}{\partial x_n} \\ \frac{\partial y_2}{\partial x_1} & \frac{\partial y_2}{\partial x_2} & \dots & \frac{\partial y_2}{\partial x_n} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial y_m}{\partial x_1} & \frac{\partial y_m}{\partial x_2} & \dots & \frac{\partial y_m}{\partial x_n} \end{bmatrix}$$

Jacobian Matrix

$$r = r(x)$$

$$\dot{r} = \frac{\partial r}{\partial x} \dot{x} = E_p(x) \dot{x}$$

Cartesian coordinates, as mentioned.

$$x_{pc} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

$$E_{pc}(x_{pc}) = E_{pc}^{-1}(x_{pc}) = I$$

Cylindrical coordinates, from matrix calculus

$$r = \begin{pmatrix} \rho \cos \theta \\ \rho \sin \theta \\ z \end{pmatrix}$$

$$x_{ps} = \begin{pmatrix} \rho \\ \theta \\ z \end{pmatrix}$$

$$E_{ps}(x_{ps}) = \frac{\partial r(x_{ps})}{\partial x_{ps}} = \begin{bmatrix} \frac{\partial r(x_{ps})_1}{\partial x_{ps1}} & \frac{\partial r(x_{ps})_1}{\partial x_{ps2}} & \frac{\partial r(x_{ps})_1}{\partial x_{ps3}} \\ \frac{\partial r(x_{ps})_2}{\partial x_{ps1}} & \frac{\partial r(x_{ps})_2}{\partial x_{ps2}} & \frac{\partial r(x_{ps})_2}{\partial x_{ps3}} \\ \frac{\partial r(x_{ps})_3}{\partial x_{ps1}} & \frac{\partial r(x_{ps})_3}{\partial x_{ps2}} & \frac{\partial r(x_{ps})_3}{\partial x_{ps3}} \end{bmatrix}$$

$$= \begin{bmatrix} \cos \theta & -\rho \sin \theta & 0 \\ \sin \theta & \rho \cos \theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

spherical coordinates

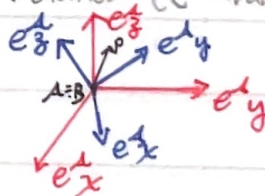
$$r = \begin{pmatrix} r \sin \phi \cos \theta \\ r \sin \phi \sin \theta \\ r \cos \phi \end{pmatrix}$$

$$x_{ps} = \begin{pmatrix} r \\ \theta \\ \phi \end{pmatrix}$$

$$E_{ps}(x_{ps}) = \frac{\partial r(x_{ps})}{\partial x_{ps}}$$

$$= \begin{bmatrix} \sin \phi \cos \theta & -r \sin \phi \sin \theta & r \cos \phi \cos \theta \\ \sin \phi \sin \theta & r \sin \phi \cos \theta & r \cos \phi \sin \theta \\ \cos \phi & 0 & -r \sin \phi \end{bmatrix}$$

rotation transformation



$$A_{AP} = \begin{pmatrix} A_{APx} & e_x^A \\ A_{APy} & e_y^A \\ A_{APz} & e_z^A \end{pmatrix}$$

$$B_{AP} = \begin{pmatrix} B_{APx} & e_x^B \\ B_{APy} & e_y^B \\ B_{APz} & e_z^B \end{pmatrix}$$

$$A_{AP} = 1 e_x^B B_{APx} + 1 e_y^B B_{APy} + 1 e_z^B B_{APz}$$

vector basis of B frame in A frame

$$= [1 e_x^B \quad 1 e_y^B \quad 1 e_z^B] B_{AP}$$

$$= C_{AB} B_{AP}$$

$$\therefore A_{AP} = C_{AB} B_{AP}$$

what's this? orthonormal group $SO(3)$

No

Date

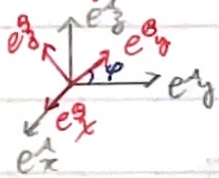
$${}^A r_{AP} = C_{AB} \otimes r_{BP}$$

$$C_{BA} = C_{AB}^{-1} = C_{AB}^T \quad (SO(3))$$

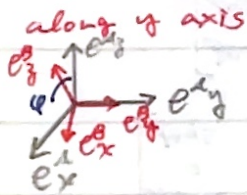
matrix is orthogonal

Above shows passive rotation (different frame)
 \downarrow
 active (same frame)

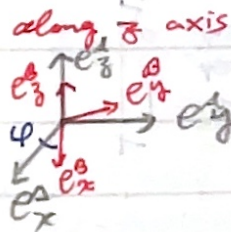
Elementary Rotation = $C_{AB} = \begin{bmatrix} e_x^B & e_y^B & e_z^B \end{bmatrix}$
 along X axis
 \hookrightarrow unit vector expressed in other frame (B in A frame)



$$C_{AB} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\phi & -\sin\phi \\ 0 & \sin\phi & \cos\phi \end{bmatrix}$$



$$C_{AB} = \begin{bmatrix} \cos\phi & 0 & \sin\phi \\ 0 & 1 & 0 \\ -\sin\phi & 0 & \cos\phi \end{bmatrix}$$



$$C_{AB} = \begin{bmatrix} \cos\phi & -\sin\phi & 0 \\ \sin\phi & \cos\phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

\therefore Homogeneous Transformation = rotation + translation

$$r_{AP} = r_{AB} + r_{BP}$$

$$\Rightarrow {}^A r_{AP} = {}^A r_{AB} + {}^A r_{BP} = {}^A r_{AB} + C_{AB} \otimes r_{BP}$$

$$\Rightarrow \begin{pmatrix} {}^A r_{AP} \\ 1 \end{pmatrix} = \begin{bmatrix} C_{AB} & {}^A r_{AB} \\ 0_{1 \times 3} & 1 \end{bmatrix} \begin{pmatrix} r_{BP} \\ 1 \end{pmatrix}$$

$T =$

$$= C_{AB}^{-1} \otimes r_{AB} \quad T^{-1} = \begin{bmatrix} C_{AB}^T & -C_{AB}^T {}^A r_{AB} \\ 0_{1 \times 3} & 1 \end{bmatrix}$$

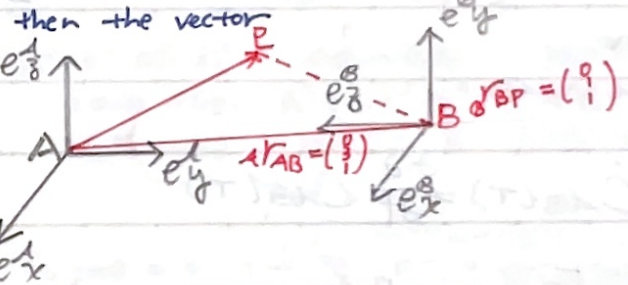
$$= -\otimes r_{AB}$$

$$= \otimes r_{BA}$$

ex. 1-3

find ${}^A r_{AP}$

find T



rotate along X axis $90^\circ (\frac{\pi}{4})$

$$C_{AB} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos 90^\circ & -\sin 90^\circ \\ 0 & \sin 90^\circ & \cos 90^\circ \end{bmatrix}$$

$$T = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos 90^\circ & -\sin 90^\circ & 3 \\ 0 & \sin 90^\circ & \cos 90^\circ & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^A r_{AP} = T_{AB} \otimes r_{BP}$$

$$= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 3 \\ 0 & 1 & 0 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} 0 \\ 1 \\ 1 \\ 1 \end{pmatrix}$$

$$= \begin{pmatrix} 0 \\ 2 \\ 2 \\ 1 \end{pmatrix}$$

$${}^A r_{AP} = [0, 2, 2]^T$$

angular velocities

${}^A \omega_{AB}$:= relative rotational velocity of B w.r.t A in A frame

$$\therefore {}^A \omega_{AB} = -{}^A \omega_{BA}$$

given Rotation Matrix $C_{AB}(t)$

angular velocity is

$${}^A \omega_{AB} = \begin{pmatrix} \omega_x \\ \omega_y \\ \omega_z \end{pmatrix}$$

where

skew-symmetric matrix

$$[{}^A \omega_{AB}]_x = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & -\omega_x \\ -\omega_y & \omega_x & 0 \end{bmatrix} = \dot{C}_{AB} C_{AB}^T$$

$${}^B \omega_{AB} = C_{BA} {}^A \omega_{AB}$$

ex. 1-4

$$\text{given } C_{AB}(t) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\alpha(t)) & \sin(\alpha(t)) \\ 0 & -\sin(\alpha(t)) & \cos(\alpha(t)) \end{bmatrix}$$

determine

1. \dot{W}_{AB}

$$\dot{C}_{AB}(t) = \frac{\partial}{\partial t} C_{AB}(t)$$

$$\Rightarrow \begin{bmatrix} 0 & 0 & 0 \\ 0 & -\sin(\alpha(t)) \dot{\alpha}(t) & \cos(\alpha(t)) \dot{\alpha}(t) \\ 0 & -\cos(\alpha(t)) \dot{\alpha}(t) & -\sin(\alpha(t)) \dot{\alpha}(t) \end{bmatrix}$$

 $C_{AB}^T(t)$

$$= \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos(\alpha(t)) & -\sin(\alpha(t)) \\ 0 & \sin(\alpha(t)) & \cos(\alpha(t)) \end{bmatrix}$$

$$\dot{C}_{AB}(t) \cdot C_{AB}^T(t)$$

$$= \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \dot{\alpha}(t) \\ 0 & -\dot{\alpha}(t) & 0 \end{bmatrix} \therefore \dot{W}_{AB} = \begin{pmatrix} -\dot{\alpha}(t) \\ 0 \\ 0 \end{pmatrix}$$

Parameterization of 3D rotation & Quaternion

now we try to parameterize rotation, similar to position (R^3)

$$\text{Rotation Matrix } C_{AB} = \begin{bmatrix} a e_x^B & a e_y^B & a e_z^B \end{bmatrix}_{R^3}$$

Orthogonality

Parameterization

Euler Angle

Angle Axis

Rotation Vector

Quaternions

} singularity issue

→ non-singular

Euler Angle

Recall: Elementary Rotation

$$C_{AB} = C_x(\varphi) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\varphi & -\sin\varphi \\ 0 & \sin\varphi & \cos\varphi \end{bmatrix}$$

$$= C_y(\varphi) = \begin{bmatrix} \cos\varphi & 0 & \sin\varphi \\ 0 & 1 & 0 \\ -\sin\varphi & 0 & \cos\varphi \end{bmatrix}$$

$$= C_z(\varphi) = \begin{bmatrix} \cos\varphi & -\sin\varphi & 0 \\ \sin\varphi & \cos\varphi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

△ Euler Angle Rotation Order

ZYZ & ZXZ proper Euler Angle

ZYX

XYZ

Tait-Bryan Angle UAV Airplane
Cardan Angle marine Apps.

ZYZ

$$C_{AB} = C_{AB}(\gamma, \text{Euler-ZYZ})$$

$$= C_{AB}(\beta_1) C_{AB}(\gamma) C_{AB}(\beta_2)$$

$$\Rightarrow \gamma = C_{AB} \alpha$$

$$\Rightarrow C_{AB}$$

$$= \begin{bmatrix} \cos\beta_1 & -\sin\beta_1 & 0 \\ \sin\beta_1 & \cos\beta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos\gamma & 0 & \sin\gamma \\ 0 & 1 & 0 \\ \sin\gamma & 0 & \cos\gamma \end{bmatrix} \begin{bmatrix} \cos\beta_2 & -\sin\beta_2 & 0 \\ \sin\beta_2 & \cos\beta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} C_{\beta_1} C_{\beta_2} - S_{\beta_1} S_{\beta_2} & -C_{\beta_2} S_{\beta_1} - C_{\beta_1} S_{\beta_2} & C_{\beta_1} S_{\beta_2} \\ C_{\beta_1} S_{\beta_2} + C_{\beta_2} S_{\beta_1} & C_{\beta_1} C_{\beta_2} - C_{\beta_2} S_{\beta_1} S_{\beta_2} & S_{\beta_1} S_{\beta_2} \\ -C_{\beta_2} S_{\beta_1} & S_{\beta_1} S_{\beta_2} & C_{\beta_1} \end{bmatrix}$$

$$= \begin{bmatrix} C_{11} & C_{12} & C_{13} \\ C_{21} & C_{22} & C_{23} \\ C_{31} & C_{32} & C_{33} \end{bmatrix} (\gamma \rightarrow C)$$

get rotation from γ

$$\chi_{R, \text{Euler-ZYZ}} = \begin{pmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \end{pmatrix} \text{ or } \chi \text{ from rotation}$$

$$= \begin{pmatrix} \text{atan2}(C_{23}, C_{13}) \\ \text{atan2}(\sqrt{C_{13}^2 + C_{23}^2}, C_{33}) \\ \text{atan2}(C_{32}, -C_{31}) \end{pmatrix} \quad (C \rightarrow \chi)$$

ZYX

$$C_{AD} = C_{AD}(\chi_{R, \text{Euler-ZYX}})$$

$$= C_{AB}(\beta) C_{AB}(y) C_{AB}(x)$$

$$= \begin{bmatrix} \cos\beta & -\sin\beta & 0 \\ \sin\beta & \cos\beta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \cos\gamma & 0 & \sin\gamma \\ 0 & 1 & 0 \\ -\sin\gamma & 0 & \cos\gamma \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\alpha & -\sin\alpha \\ 0 & \sin\alpha & \cos\alpha \end{bmatrix}$$

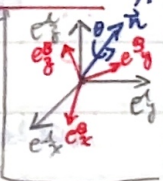
$$= \begin{bmatrix} C_{\beta}C_{\gamma} & C_{\beta}S_{\gamma}S_{\alpha} - C_{\alpha}S_{\beta} & S_{\alpha}S_{\beta} + C_{\alpha}C_{\beta}S_{\gamma} \\ C_{\gamma}S_{\beta} & C_{\alpha}C_{\beta} + S_{\alpha}S_{\beta}S_{\gamma} & C_{\alpha}S_{\beta}S_{\gamma} - C_{\gamma}S_{\alpha} \\ -S_{\gamma} & C_{\gamma}S_{\alpha} & C_{\alpha}C_{\gamma} \end{bmatrix} \begin{matrix} x \\ y \\ z \end{matrix}$$

$$\chi_{R, \text{Euler-ZYX}} = \begin{pmatrix} \beta_1 \\ \beta_2 \\ \beta_3 \end{pmatrix} = \begin{pmatrix} \text{atan2}(C_{21}, -C_{11}) \\ \text{atan2}(-C_{31}, \sqrt{C_{32}^2 + C_{33}^2}) \\ \text{atan2}(C_{32}, C_{33}) \end{pmatrix} \quad (C \rightarrow \chi)$$

Angle axis

$$\chi_{R, \text{Angle axis}} = \begin{pmatrix} \theta \\ n \end{pmatrix} \begin{matrix} \text{rotation angle} \\ \text{rotation axis} \end{matrix}$$

Rotation vector = $\varphi = \theta \cdot n$ (R²)
aka Euler vectors



$$C_{AB}(\theta, n) = \cos\theta \cdot I_{3 \times 3} - \sin\theta [n]_{\times} + (1 - \cos\theta)nn^T$$

$$\Rightarrow \begin{bmatrix} n_x^2(1 - \cos\theta) + \cos\theta & n_x n_y(1 - \cos\theta) - n_z s_{\theta} & n_x n_z(1 - \cos\theta) + n_y s_{\theta} \\ n_x n_y(1 - \cos\theta) + n_z s_{\theta} & n_y^2(1 - \cos\theta) + \cos\theta & n_y n_z(1 - \cos\theta) - n_x s_{\theta} \\ n_x n_z(1 - \cos\theta) - n_y s_{\theta} & n_y n_z(1 - \cos\theta) + n_x s_{\theta} & n_z^2(1 - \cos\theta) + \cos\theta \end{bmatrix}$$

($\chi \rightarrow C$)

$$\theta = \cos^{-1} \left(\frac{C_{11} + C_{22} + C_{33} - 1}{2} \right)$$

$$n = \frac{1}{2 \sin\theta} \begin{pmatrix} C_{32} - C_{23} \\ C_{13} - C_{31} \\ C_{21} - C_{12} \end{pmatrix}$$

singularity

Unit Quaternions

complex numbers in 4D $\hat{q} = \hat{q}_0 + \hat{q}_1 i + \hat{q}_2 j + \hat{q}_3 k$

Hamiltonian convention $j^2 = j^2 = k^2 = ijk = -1$

Scalar

vector

$$\chi_{R, \text{quat}} = \hat{q} = \begin{pmatrix} \hat{q}_0 \\ \hat{q}_1 \\ \hat{q}_2 \\ \hat{q}_3 \end{pmatrix} \in \mathbb{H}$$

Real part $\hat{q}_0 = \cos \frac{\|\varphi\|}{2} = \cos \left(\frac{\theta}{2} \right)$

Imaginary $\hat{q} = \sin \frac{\|\varphi\|}{2} \cdot \frac{\varphi}{\|\varphi\|} = \sin \left(\frac{\theta}{2} \right) n = \begin{pmatrix} \hat{q}_1 \\ \hat{q}_2 \\ \hat{q}_3 \end{pmatrix}$

Unitary Constraint $\hat{q}_0^2 + \hat{q}_1^2 + \hat{q}_2^2 + \hat{q}_3^2 = 1$

Inverse $\hat{q}^{-1} \Leftrightarrow \hat{q}^T = \begin{pmatrix} \hat{q}_0 \\ -\hat{q}_1 \\ -\hat{q}_2 \\ -\hat{q}_3 \end{pmatrix}$

Identity $y = (1 \ 0 \ 0 \ 0)^T \quad (\theta = 0)$

Rotation Matrix

$$C_{AD} = I_{3 \times 3} + 2\hat{q}_0 [\hat{q}]_{\times} + 2[\hat{q}]_{\times}^2$$

$$= (2\hat{q}_0^2 - 1) I_{3 \times 3} + 2\hat{q}_0 [\hat{q}]_{\times} + 2\hat{q} \hat{q}^T$$

$$\begin{bmatrix} 2\hat{q}_0^2 + \hat{q}_1^2 - \hat{q}_2^2 - \hat{q}_3^2 & 2\hat{q}_1\hat{q}_2 - 2\hat{q}_0\hat{q}_3 & 2\hat{q}_0\hat{q}_2 + 2\hat{q}_1\hat{q}_3 \\ 2\hat{q}_0\hat{q}_3 + 2\hat{q}_1\hat{q}_2 & \hat{q}_0^2 - \hat{q}_1^2 + \hat{q}_2^2 - \hat{q}_3^2 & 2\hat{q}_2\hat{q}_3 - 2\hat{q}_0\hat{q}_1 \\ 2\hat{q}_1\hat{q}_3 - 2\hat{q}_0\hat{q}_2 & 2\hat{q}_0\hat{q}_1 + 2\hat{q}_2\hat{q}_3 & \hat{q}_0^2 - \hat{q}_1^2 - \hat{q}_2^2 + \hat{q}_3^2 \end{bmatrix}$$

$\chi \rightarrow C$

$$\chi_{R, \text{quat}} = \hat{q} = \frac{1}{2} \begin{pmatrix} C_{11} + C_{22} + C_{33} + 1 \\ \text{sgn}(C_{22} - C_{33}) \sqrt{C_{11} - C_{22} - C_{33} + 1} \\ \text{sgn}(C_{13} - C_{31}) \sqrt{C_{22} - C_{33} - C_{11} + 1} \\ \text{sgn}(C_{21} - C_{12}) \sqrt{C_{33} - C_{11} - C_{22} + 1} \end{pmatrix}$$

$C \rightarrow \chi$

Quaternions Algebra

$$\hat{q} \otimes P = (\hat{q}_0 + \hat{q}_1 i + \hat{q}_2 j + \hat{q}_3 k) (P_0 + P_1 i + P_2 j + P_3 k)$$

$$= \hat{q}_0 P_0 + \hat{q}_0 P_1 i + \hat{q}_0 P_2 j + \hat{q}_0 P_3 k$$

$$+ \hat{q}_1 P_0 i + \hat{q}_1 P_1 ii + \hat{q}_1 P_2 ij + \hat{q}_1 P_3 ik$$

$$+ \hat{q}_2 P_0 j + \hat{q}_2 P_1 ji + \hat{q}_2 P_2 jj + \hat{q}_2 P_3 jk$$

$$+ \hat{q}_3 P_0 k + \hat{q}_3 P_1 ki + \hat{q}_3 P_2 kj + \hat{q}_3 P_3 kk$$

$$\left(\begin{matrix} i^2 = j^2 = k^2 = ijk = -1 \\ ij = -ji = -ijk^2 = k \\ jk = -kj = i \\ ki = -ik = j \end{matrix} \right)$$

$$= \hat{q}_0 P_0 - \hat{q}_1 P_1 - \hat{q}_2 P_2 - \hat{q}_3 P_3$$

$$+ (\hat{q}_0 P_1 + \hat{q}_1 P_0 + \hat{q}_2 P_3 - \hat{q}_3 P_2) i$$

$$+ (\hat{q}_0 P_2 - \hat{q}_1 P_3 + \hat{q}_2 P_0 + \hat{q}_3 P_1) j$$

$$+ (\hat{q}_0 P_3 + \hat{q}_1 P_2 - \hat{q}_2 P_1 + \hat{q}_3 P_0) k$$

$$= \begin{bmatrix} \hat{q}_0 & -\hat{q}_1 & -\hat{q}_2 & -\hat{q}_3 \\ \hat{q}_1 & \hat{q}_0 & -\hat{q}_3 & \hat{q}_2 \\ \hat{q}_2 & \hat{q}_3 & \hat{q}_0 & -\hat{q}_1 \\ \hat{q}_3 & -\hat{q}_2 & \hat{q}_1 & \hat{q}_0 \end{bmatrix} \begin{pmatrix} P_0 \\ P_1 \\ P_2 \\ P_3 \end{pmatrix}$$

$$= \begin{bmatrix} \hat{q}_0 & -\hat{q}^T \\ \hat{q} & \hat{q}_0 I + [\hat{q}]_{\times} \end{bmatrix} P = m_{\ell}(\hat{q}) P$$

$:= m_{\ell}(\hat{q})$

$$= \begin{bmatrix} P_0 & -P_1 & -P_2 & -P_3 \\ P_1 & P_0 & P_3 & -P_2 \\ P_2 & -P_3 & P_0 & P_1 \\ P_3 & P_2 & -P_1 & P_0 \end{bmatrix} \begin{pmatrix} \hat{q}_0 \\ \hat{q}_1 \\ \hat{q}_2 \\ \hat{q}_3 \end{pmatrix}$$

$:= m_r(P)$

$$= \begin{bmatrix} P_0 & -\hat{P}^T \\ \hat{P} & P_0 I - [\hat{P}]_{\times} \end{bmatrix} \hat{q} = m_r(P) \hat{q}$$

$$(w_1 + v_1^T) (w_2 + v_2^T)$$

$$= (w_1 \cdot w_2 - v_1^T \cdot v_2^T - w_1 v_2^T + w_2 v_1^T + v_1^T \times v_2^T)$$

Using Quaternion to rotate a vector

$$\mathcal{B}r = C_{BI} \mathcal{I}r$$

write $\mathcal{I}r$ into Quaternion (as the imaginary part of ξ)

$$P(\mathcal{I}r) = \begin{pmatrix} 0 \\ \mathcal{I}r \end{pmatrix} \rightarrow \text{unit quaternion}$$

$$\therefore P(\mathcal{B}r) = \zeta_{BI} \otimes P(\mathcal{I}r) \otimes \zeta_{BI}^T$$

$$\mathcal{B}r = C_{BI} \mathcal{I}r$$

$$P(\mathcal{B}r) = \zeta \otimes P(\mathcal{I}r) \otimes \zeta^T = M_L(\zeta) M_R(\zeta^T) (\mathcal{I}r)$$

$$\Rightarrow \begin{pmatrix} 0 \\ \mathcal{B}r \end{pmatrix} = \begin{bmatrix} \zeta_0 & -\zeta^T \\ \zeta & \zeta_0 I + [\zeta]_x \end{bmatrix} \begin{bmatrix} \zeta_0 & \zeta^T \\ -\zeta & \zeta_0 I + [\zeta]_x \end{bmatrix} \begin{pmatrix} 0 \\ \mathcal{I}r \end{pmatrix}$$

$$= \begin{bmatrix} \zeta_0^2 + |\zeta|^2 & 0 \\ \zeta_0 \zeta - \zeta_0 \zeta - [\zeta]_x \zeta & \zeta \zeta^T + \zeta_0^2 I + 2\zeta_0 [\zeta]_x + [\zeta]_x [\zeta]_x \end{bmatrix} \begin{pmatrix} 0 \\ \mathcal{I}r \end{pmatrix}$$

$$M_L(\zeta) = \begin{bmatrix} \zeta_0 & -\zeta^T \\ \zeta & \zeta_0 I + [\zeta]_x \end{bmatrix}$$

$$[\zeta^T]_x = -[\zeta]_x \quad \zeta^{-1} = \zeta^T = \begin{pmatrix} \zeta_0 \\ -\zeta \end{pmatrix}$$

$$\begin{aligned} -\zeta^T [\zeta]_x &= -\zeta^T (-[\zeta^T]_x) = \zeta \zeta^T - |\zeta|^2 I \\ &= 0 \end{aligned}$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & (\zeta_0^2 - |\zeta|^2) I + 2\zeta_0 [\zeta]_x + 2\zeta \zeta^T \end{bmatrix}$$

$$\begin{pmatrix} 0 \\ \mathcal{B}r \end{pmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & (\zeta_0^2 - |\zeta|^2) I + 2\zeta_0 [\zeta]_x + 2\zeta \zeta^T \end{bmatrix} \begin{pmatrix} 0 \\ \mathcal{I}r \end{pmatrix}$$

$$\therefore \mathcal{B}r = ((\zeta_0^2 - |\zeta|^2) I + 2\zeta_0 [\zeta]_x + 2\zeta \zeta^T) \mathcal{I}r$$

$C(\zeta)$

Time Derivatives

$$\omega_{AD} \Leftrightarrow \dot{\chi}_{AD}$$

recall:

$$\dot{r} = E_p(x) \dot{\chi}$$

Now:

$$\omega_{AB} = E_R(\chi_R) \dot{\chi}_R$$

Find this

$$\omega_{AB} = E_R(\chi_R) \dot{\chi}_R$$

Take ZYX Euler angle for example

$$\omega_{AB} = \omega_{AB} + \omega_{BC} + \omega_{CD}$$

$$= \omega_{AB} + C_{AB} \omega_{BC} + C_{AB} C_{BC} \omega_{CD}$$

$$= \omega_z^A \cdot \hat{z} + C_{AB} \omega_y^B \cdot \hat{y} + C_{AB} C_{BC} \omega_x^C \cdot \hat{x}$$

$$= \underbrace{\begin{bmatrix} \omega_z^A & C_{AB} \omega_y^B & C_{AB} C_{BC} \omega_x^C \end{bmatrix}}_{E_R(\chi_R)} \begin{pmatrix} \hat{x} \\ \hat{y} \\ \hat{z} \end{pmatrix}$$

$$C_{AB} \omega_y^B = \begin{bmatrix} c_{\beta} & -s_{\beta} & 0 \\ s_{\beta} & c_{\beta} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \begin{pmatrix} -s_{\beta} \\ c_{\beta} \\ 0 \end{pmatrix}$$

$$C_{AB} C_{BC} \omega_x^C = \begin{bmatrix} c_{\beta} & -s_{\beta} & 0 \\ s_{\beta} & c_{\beta} & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} c_{\alpha} & 0 & s_{\alpha} \\ 0 & 1 & 0 \\ -s_{\alpha} & 0 & c_{\alpha} \end{bmatrix} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} c_{\alpha} c_{\beta} \\ c_{\alpha} s_{\beta} \\ -s_{\alpha} \end{pmatrix}$$

$$\therefore E_R(\chi_R) = \begin{bmatrix} 0 & -s_{\beta} & c_{\alpha} c_{\beta} \\ 0 & c_{\beta} & c_{\alpha} s_{\beta} \\ 1 & 0 & -s_{\alpha} \end{bmatrix}$$

$$\omega_{AB} = \begin{bmatrix} 0 & -s_{\beta} & c_{\alpha} c_{\beta} \\ 0 & c_{\beta} & c_{\alpha} s_{\beta} \\ 1 & 0 & -s_{\alpha} \end{bmatrix} \dot{\chi}_R$$

$$\det(E_R) = -\cos(\beta) \text{ (singularity)}$$

Angle Axis $\begin{pmatrix} \theta \\ n \end{pmatrix}$

$$E_{R, \text{angle axis}} = [n \sin \theta I_{3 \times 3} + (1 - \cos \theta) [n]_x]$$

$$E_{R, \text{angle axis}}^{-1} = \begin{bmatrix} n^T \\ -\frac{1}{2} \frac{\sin \theta}{1 - \cos \theta} [n]_x^2 - \frac{1}{2} [n]_x \end{bmatrix}$$

Rotation Vector $(\varphi = \theta n)$

$$E_{R, \text{rotation vector}} = [I_{3 \times 3} + [\varphi]_x \left(\frac{1 - \cos \|\varphi\|}{\|\varphi\|^2} \right) + [\varphi]_x^2 \left(\frac{1 - \cos \|\varphi\|}{\|\varphi\|^4} \right)]$$

$$E_{R, \text{rotation vector}}^{-1} = [I_{3 \times 3} - \frac{1}{2} [\varphi]_x + [\varphi]_x^2 \frac{1}{\|\varphi\|^2} \left(1 - \frac{\|\varphi\| \sin \|\varphi\|}{2(1 - \cos \|\varphi\|)} \right)]$$

Quaternion

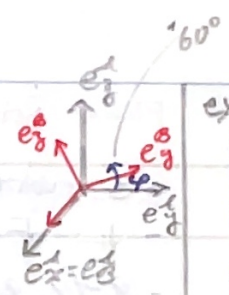
$$E_{R, \text{quat}} = 2H(\xi)$$

$$E_{R, \text{quat}}^{-1} = \frac{1}{2} H(\xi)^T \quad w/ \quad H(\xi) = \begin{bmatrix} -\xi & [\xi]_x + \xi_0 I_{3 \times 3} \end{bmatrix}$$

$$= \begin{bmatrix} -\xi_1 & \xi_0 & -\xi_3 & \xi_2 \\ -\xi_2 & \xi_3 & \xi_0 & -\xi_1 \\ -\xi_3 & -\xi_2 & \xi_1 & \xi_0 \end{bmatrix}$$

ex. 2-1

Find Rotation Matrix C_{AB}
Euler ZYX
Angle Axis
Quaternions



$$C_{AB} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos 60^\circ & -\sin 60^\circ \\ 0 & \sin 60^\circ & \cos 60^\circ \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 & 0 \\ 0 & \frac{1}{2} & -\frac{\sqrt{3}}{2} \\ 0 & \frac{\sqrt{3}}{2} & \frac{1}{2} \end{bmatrix} \quad \text{**}$$

Euler ZYX

$$R_{R, \text{Euler ZYX}} = \begin{pmatrix} \alpha \\ \beta \\ \gamma \end{pmatrix} = \begin{pmatrix} \text{atan2}(C_{21}, C_{11}) \\ \text{atan2}(-C_{31}, \sqrt{C_{32}^2 + C_{33}^2}) \\ \text{atan2}(C_{32}, C_{33}) \end{pmatrix}$$

$$= \begin{pmatrix} \text{atan2}(0, 1) \\ \text{atan2}(-0, \sqrt{(\sqrt{3}/2)^2 + (1/2)^2}) \\ \text{atan2}(\sqrt{3}/2, 1/2) \end{pmatrix}$$

$$= \begin{pmatrix} 0 \\ 0 \\ 60^\circ \end{pmatrix} \quad \text{**}$$

Angle Axis

$$\theta = \cos^{-1} \left(\frac{C_{11} + C_{22} + C_{33} - 1}{2} \right)$$

$$= \cos^{-1} \left(\frac{1 + \cos 60^\circ + \cos 60^\circ - 1}{2} \right)$$

$$= \cos^{-1}(\cos 60^\circ) = 60^\circ \quad \text{**}$$

$$n = \frac{1}{2 \sin(\theta)} \begin{pmatrix} C_{32} - C_{23} \\ C_{13} - C_{31} \\ C_{21} - C_{12} \end{pmatrix} = \frac{1}{2 \sin 60^\circ} \begin{pmatrix} \sin 60^\circ - (-\sin 60^\circ) \\ 0 \\ 0 \end{pmatrix}$$

$$= \frac{1}{2 \sin 60^\circ} \begin{pmatrix} 2 \sin 60^\circ \\ 0 \\ 0 \end{pmatrix}$$

$$= \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \quad \text{**}$$

Quaternions

$$R_{R, \text{quat}} = \frac{1}{2} \begin{pmatrix} \text{sgn}(C_{32} - C_{23}) \sqrt{\frac{C_{11} + C_{22} + C_{33} + 1}{2}} \\ \text{sgn}(C_{13} - C_{31}) \sqrt{\frac{C_{22} - C_{33} - C_{11} + 1}{2}} \\ \text{sgn}(C_{21} - C_{12}) \sqrt{\frac{C_{33} - C_{11} - C_{22} + 1}{2}} \\ 0 \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} \sqrt{1 + \cos 60^\circ + \cos 60^\circ + 1} \\ + \sqrt{1 - \cos 60^\circ - \cos 60^\circ + 1} \\ 0 \cdot \sqrt{\cos 60^\circ - \cos 60^\circ - 1 + 1} \\ 0 \cdot \sqrt{\cos 60^\circ - 1 - \cos 60^\circ + 1} \end{pmatrix}$$

$$= \frac{1}{2} \begin{pmatrix} \sqrt{3} \\ 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} \frac{\sqrt{3}}{2} \\ \frac{1}{2} \\ 0 \\ 0 \end{pmatrix} = \xi_{AB} \quad \text{**}$$

ex. 2-2

Based upon ex. 2-1 $r = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$ in A frame
Rotate w/ quaternions to B frame
Rotate directly w/ complex numbers to B frame

$$P(r) = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \xi_{BA} \otimes P(r) \otimes \xi_{BA}^T$$

$$= M_{\xi}(\xi_{BA}) M_R(\xi_{BA}^T) \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

from previous: $\xi_{AB} = \frac{1}{2} \begin{pmatrix} \sqrt{3} \\ 1 \\ 0 \\ 0 \end{pmatrix}$

$\therefore \xi_{BA} = \frac{1}{2} \begin{pmatrix} \sqrt{3} \\ 1 \\ 0 \\ 0 \end{pmatrix} \cos \frac{\theta}{2} + \dots$

$$M_{\xi}(\xi) = \begin{bmatrix} \xi_0 & -\xi_1 & -\xi_2 & -\xi_3 \\ \xi_1 & \xi_0 & -\xi_3 & \xi_2 \\ \xi_2 & \xi_3 & \xi_0 & -\xi_1 \\ \xi_3 & -\xi_2 & \xi_1 & \xi_0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sqrt{3} & 1 & 0 & 0 \\ -1 & \sqrt{3} & 0 & 0 \\ 0 & 0 & \sqrt{3} & 1 \\ 0 & 0 & -1 & \sqrt{3} \end{bmatrix}$$

$$\xi_{BA}^T = \xi_{BA}^{-1} = \begin{pmatrix} \xi_0 \\ -\xi_1 \\ -\xi_2 \\ \xi_3 \end{pmatrix} = \frac{1}{2} \begin{pmatrix} \sqrt{3} \\ 1 \\ 0 \\ 0 \end{pmatrix}$$

$$M_R(\xi) = \begin{bmatrix} \xi_0 & -\xi_1 & -\xi_2 & -\xi_3 \\ \xi_1 & \xi_0 & \xi_3 & -\xi_2 \\ \xi_2 & -\xi_3 & \xi_0 & \xi_1 \\ \xi_3 & \xi_2 & -\xi_1 & \xi_0 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \sqrt{3} & -1 & 0 & 0 \\ 1 & \sqrt{3} & 0 & 0 \\ 0 & 0 & \sqrt{3} & 1 \\ 0 & 0 & -1 & \sqrt{3} \end{bmatrix}$$

$$P(r) = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \frac{1}{2} \begin{bmatrix} \sqrt{3} & 1 & 0 & 0 \\ -1 & \sqrt{3} & 0 & 0 \\ 0 & 0 & \sqrt{3} & 1 \\ 0 & 0 & -1 & \sqrt{3} \end{bmatrix} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$= \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \quad \text{**}$$

$$r = \begin{pmatrix} 0 \\ \frac{1}{2} \\ -\frac{\sqrt{3}}{2} \end{pmatrix} \quad \text{**}$$

$$P(r) = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} = \xi_{BA} \otimes P(r) \otimes \xi_{BA}^T \quad \left(\xi_{BA} = \frac{1}{2} \begin{pmatrix} \sqrt{3} \\ 1 \\ 0 \\ 0 \end{pmatrix} \right)$$

$$= \left(\frac{1}{2}(\sqrt{3} - i) \right) (j) \left(\frac{1}{2}(\sqrt{3} + i) \right)$$

$$= \left(\frac{\sqrt{3}}{2} - \frac{i}{2} \right) j \left(\frac{\sqrt{3}}{2} + \frac{i}{2} \right)$$

$$= \left(\frac{\sqrt{3}}{2} j - \frac{j^2}{2} \right) \left(\frac{\sqrt{3}}{2} + \frac{i}{2} \right)$$

$$= \frac{3}{4} j + \frac{\sqrt{3}}{4} j^2 - \frac{\sqrt{3}}{4} j - \frac{j^2}{4}$$

$$= \frac{3}{4} j - \frac{\sqrt{3}}{4} j - \frac{\sqrt{3}}{4} j - \frac{j^2}{4}$$

$$= \frac{3}{4} j - \frac{\sqrt{3}}{2} j - \frac{j^2}{4}$$

$$= \frac{3}{4} j - \frac{\sqrt{3}}{2} j - \frac{j^2}{4}$$

$$= \frac{1}{2} j - \frac{\sqrt{3}}{2} j \quad \left(\begin{pmatrix} 0 \\ \frac{1}{2} \\ -\frac{\sqrt{3}}{2} \end{pmatrix} \right) \quad \text{**}$$

Kinematics

Fixed-base system

n_j joints (revolute, prismatic)

$n_l = n_j + 1$ links

n_j moving links

1 fixed link

A Robot Arm example



n moving links $6n$ parameters

n IDoF joints $5n$ parameters

$6n - 5n = n$ DoFs

$$q = \begin{pmatrix} q_1 \\ \vdots \\ q_{n_j} \end{pmatrix} \in \mathbb{R}^{n_j}$$

complete independent not unique

generalized coordinates

End-effectors

(task space)

$$x_e = \begin{pmatrix} x_{eP} \\ x_{eR} \end{pmatrix} = \begin{pmatrix} x_1 \\ \vdots \\ x_m \end{pmatrix} \in \mathbb{R}^m$$

to I (inertial frame)

Operation space coordinates (the "real" DoF) @ end-effectors

$$x_0 = \begin{pmatrix} x_{0P} \\ x_{0R} \end{pmatrix} = \begin{pmatrix} x_1 \\ \vdots \\ x_{m_0} \end{pmatrix}$$

DoF @ end-effectors

ex. 3-1

- 1 Most general robot arm
 - 2 SCARA robot arm
 - 3 ANYpulator (4 joints)
- get q, m_e, x_e, m_0, x_0

$$q = (q_1, q_2, q_3, q_4, q_5, q_6)$$

$$m_e = 6$$

$$x_e = (x, y, z, \alpha_x, \beta_y, r_z)$$

$$m_0 = 6$$

$$x_0 = (x, y, z, \alpha_x, \beta_y, r_z)$$

$$2. q = (\alpha, \beta, r, \gamma)$$

$$m_e = 6$$

$$x_e = (x, y, z, \alpha_x, \beta_y, r_z)$$

$$m_0 = 4$$

$$x_0 = (x, y, z, r_z)$$

$$3. q = (q_1, q_2, q_3, q_4)$$

$$m_e = 6$$

$$x_e = (x, y, z, \alpha_x, \beta_y, r_z)$$

$$m_0 = 4$$

$x_0 =$ hard to pick

Planar Robot Arm

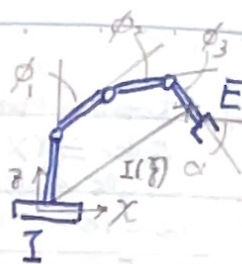
- 3 revolute joints

- 1 end-effector

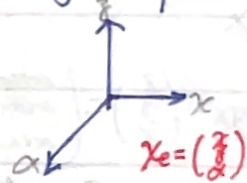
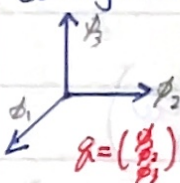
$$q = (q_1, q_2, q_3) \in \mathbb{R}^3$$

$m_e = 3$

$$x_e = (x, y, \alpha)$$



configuration space \leftrightarrow joint space (generalize)



map to one and another

End-effector

$$x_e = x_e(q) \in \mathbb{R}^{m_e}$$

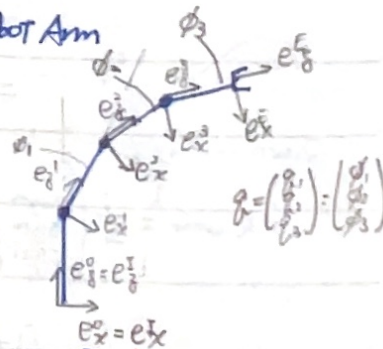
Transformation Matrix from E to I

$$T_{IE}(q) = T_{I0} \cdot \prod_{k=1}^{n_j} T_{k-1,k}(q_k) \cdot T_{n,n_e}$$

$$= \begin{bmatrix} C_{IE} & I_{IE} \\ 0_{1 \times 3} & I \end{bmatrix}$$

ex. 3-2

Get the T_{IE} of the Robot Arm RHS.



$$T_{IE} = T_{I0} \cdot T_{01} \cdot T_{12} \cdot T_{23} \cdot T_{3E}$$

$$T_{I0} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

(recall: rotate around y)

$$C_y(\varphi) = \begin{bmatrix} \cos\varphi & 0 & \sin\varphi \\ 0 & 1 & 0 \\ -\sin\varphi & 0 & \cos\varphi \end{bmatrix}$$

$$T_{01} = \begin{bmatrix} c\phi_1 & 0 & s\phi_1 & 0 \\ 0 & 1 & 0 & 0 \\ -s\phi_1 & 0 & c\phi_1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{12} = \begin{bmatrix} c\phi_2 & 0 & s\phi_2 & 0 \\ 0 & 1 & 0 & 0 \\ -s\phi_2 & 0 & c\phi_2 & l_1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{23} = \begin{bmatrix} c\phi_3 & 0 & s\phi_3 & 0 \\ 0 & 1 & 0 & 0 \\ -s\phi_3 & 0 & c\phi_3 & l_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{3E} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & l_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$l_1 s \phi_1 + l_2 s(\phi_1 + \phi_2) + l_3 s(\phi_1 + \phi_2 + \phi_3)$$

$$l_0 + l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3)$$

(cont'd)

$$\therefore T_{IE} = T_{I0} \cdot T_{01} \cdot T_{12} \cdot T_{23} \cdot T_{3E}$$

$$T_{IE} = \begin{bmatrix} c(\phi_1 + \phi_2 + \phi_3) & 0 & s(\phi_1 + \phi_2 + \phi_3) & x \\ 0 & 1 & 0 & y \\ -s(\phi_1 + \phi_2 + \phi_3) & 0 & c(\phi_1 + \phi_2 + \phi_3) & z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$x = l_1 s \phi_1 + l_2 s(\phi_1 + \phi_2) + l_3 s(\phi_1 + \phi_2 + \phi_3)$$

$$y = 0$$

$$z = l_0 + l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3)$$

$$\therefore X_{ep}(\phi) = \begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} l_1 s \phi_1 + l_2 s(\phi_1 + \phi_2) + l_3 s(\phi_1 + \phi_2 + \phi_3) \\ 0 \\ l_0 + l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) \end{pmatrix}$$

$$X_{eR}(\phi) = (\phi_1 + \phi_2 + \phi_3)$$

Jacobians of a Robot Manipulator

recall Forward Kinematics

$$T_{IE}(\phi) = \begin{bmatrix} C_{IE}(\phi) & I_{FIE}(\phi) \\ 0_{1 \times 3} & 1 \end{bmatrix} \quad X_e = \begin{pmatrix} X_{ep} \\ X_{eR} \end{pmatrix} = V_e(\phi)$$

Forward Kinematics (Differential)

- Analytic

$$X_e + \delta X_e = X_e(\phi + \delta \phi) = X_e(\phi) + \frac{\partial X_e}{\partial \phi} \delta \phi + o(\delta \phi^2)$$

$$\therefore \delta X_e \approx \frac{\partial X_e}{\partial \phi} \delta \phi = J_{eA}(\phi) \delta \phi$$

recall Matrix Calculus

$$J_{eA} = \frac{\partial X_e}{\partial \phi} = \begin{bmatrix} \frac{\partial x_1}{\partial \phi_1} & \dots & \frac{\partial x_1}{\partial \phi_n} \\ \vdots & \ddots & \vdots \\ \frac{\partial x_m}{\partial \phi_1} & \dots & \frac{\partial x_m}{\partial \phi_n} \end{bmatrix}$$

$$\dot{X}_e = J_{eA}(\phi) \dot{\phi}$$

m_e # end-effector state
 n_j # joints
(comparing)

ex.3-3-1

From last example (ex.3-2) determine the analytic Jacobia

$$X_{ep}(\phi) = \begin{pmatrix} l_1 s \phi_1 + l_2 s(\phi_1 + \phi_2) + l_3 s(\phi_1 + \phi_2 + \phi_3) \\ l_0 + l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) \end{pmatrix}$$

$$X_{eR}(\phi) = \phi_1 + \phi_2 + \phi_3$$

$$J_{eAP}(\phi) = \frac{\partial X_{ep}(\phi)}{\partial \phi}$$

(cont'd)

$$J_{eAP}(\phi) = \frac{\partial X_{ep}(\phi)}{\partial \phi} = \begin{bmatrix} \frac{\partial X_{ep}(\phi)_1}{\partial \phi_1} & \frac{\partial X_{ep}(\phi)_1}{\partial \phi_2} & \frac{\partial X_{ep}(\phi)_1}{\partial \phi_3} \\ \frac{\partial X_{ep}(\phi)_2}{\partial \phi_1} & \frac{\partial X_{ep}(\phi)_2}{\partial \phi_2} & \frac{\partial X_{ep}(\phi)_2}{\partial \phi_3} \end{bmatrix}$$

$$= \begin{bmatrix} l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) & l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) & l_3 c(\phi_1 + \phi_2 + \phi_3) \\ -l_1 s \phi_1 - l_2 s(\phi_1 + \phi_2) - l_3 s(\phi_1 + \phi_2 + \phi_3) & -l_2 s(\phi_1 + \phi_2) - l_3 s(\phi_1 + \phi_2 + \phi_3) & -l_3 s(\phi_1 + \phi_2 + \phi_3) \end{bmatrix}$$

$$J_{eAR}(\phi) = \frac{\partial X_{eR}(\phi)}{\partial \phi} = \begin{bmatrix} \frac{\partial X_{eR}(\phi)_1}{\partial \phi_1} & \frac{\partial X_{eR}(\phi)_1}{\partial \phi_2} & \frac{\partial X_{eR}(\phi)_1}{\partial \phi_3} \end{bmatrix} = [1 \ 1 \ 1]$$

$$J_{eA} = \begin{bmatrix} l_1 c \phi_1 + l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) & l_2 c(\phi_1 + \phi_2) + l_3 c(\phi_1 + \phi_2 + \phi_3) & l_3 c(\phi_1 + \phi_2 + \phi_3) \\ -l_1 s \phi_1 - l_2 s(\phi_1 + \phi_2) - l_3 s(\phi_1 + \phi_2 + \phi_3) & -l_2 s(\phi_1 + \phi_2) - l_3 s(\phi_1 + \phi_2 + \phi_3) & -l_3 s(\phi_1 + \phi_2 + \phi_3) \end{bmatrix}$$

- Analytic

$$J_{eA}(\phi) = R^{m_e \times n_j}$$

depend on parameterization

- Geometric

$$W_e = \begin{pmatrix} V_e \\ \omega_e \end{pmatrix} = J_{e0}(\phi) \dot{\phi}$$

map from generalized to linear & angular velocity

$$J_{e0}(\phi) = R^{6 \times n_j}$$

always 6!

(recall $W_e = E_e(\dot{X}_e) \dot{\phi}$)

$$J_{e0}(\phi) = E_e(\dot{X}_e) J_{eA}(\phi)$$

$$\begin{cases} W_e = \begin{pmatrix} V_e \\ \omega_e \end{pmatrix} = W_B + W_{BC} \\ J_e \dot{\phi} = J_B \dot{\phi} + J_{BC} \dot{\phi} \\ A J_e = A J_B + A J_{BC} \end{cases} \text{algebras}$$

Derivation of Geometric Jacobian

(recall ${}^A r_{AP} = {}^A r_{AB} + {}^A r_{BP} = {}^A r_{AB} + C_{AB} \cdot B r_{BP}$)

Differentiate w/ time

$$V_P = \dot{{}^A r}_{AP} = \dot{{}^A r}_{AB} + C_{AB} B \dot{r}_{BP} + \dot{C}_{AB} \cdot B r_{BP}$$

(recall $[{}^A W_{AB}]_x = \dot{C}_{AB} C_{AB}^T$)

$$C_{BA} = C_{AB}^{-1} = C_{AB}^T$$

$$\therefore \dot{C}_{AB} = [{}^A W_{AB}]_x \cdot (C_{AB}^T)^{-1} = [{}^A W_{AB}]_x \cdot C_{AB}$$

$$\therefore \dot{{}^A r}_{AP} = \dot{{}^A r}_{AB} + C_{AB} B \dot{r}_{BP} + [{}^A W_{AB}]_x C_{AB} B r_{BP}$$

$$= \dot{{}^A r}_{AB} + [{}^A W_{AB}]_x {}^A r_{BP}$$

$$= \dot{{}^A r}_{AB} + {}^A W_{AB} \times {}^A r_{BP}$$

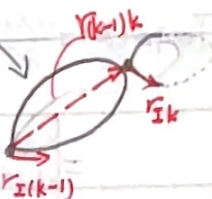
$$\therefore V_P = V_B + \Omega \times r_{BP} \text{ in } A \text{ frame}$$

(cont'd)

$v_p = v_B + \omega \times r_{BP}$ (linear). from above

$$\dot{r}_{ik} = \dot{r}_{i(k-1)} + \omega_{i(k-1)} \times r_{i(k-1)k}$$

omega of that body



consecutively

$$\dot{r}_{iE} = \sum_{k=1}^n \omega_{i,k} \times r_{k(k+1)} \quad (\text{linear})$$

as for angular

$$\omega_{i(k)} = \omega_{i(k-1)} + \omega_{(k-1)(k)}$$

$= n_k \dot{\theta}_k$ — velocity of the generalized coordinate.
normal vector of the joint

$$\therefore \omega_{i(k)} = \sum_{i=1}^k n_i \dot{\theta}_i \quad (\text{angular})$$

$$\therefore \dot{r}_{iE} = \sum_{k=1}^n \omega_{i(k)} \times r_{k(k+1)}$$

$$= \sum_{k=1}^n \left\{ \sum_{i=1}^k (n_i \dot{\theta}_i) \times r_{k(k+1)} \right\}$$

$$= n_1 \dot{\theta}_1 \times r_{12} + (n_1 \dot{\theta}_1 + n_2 \dot{\theta}_2) \times r_{23} + (n_1 \dot{\theta}_1 + n_2 \dot{\theta}_2 + n_3 \dot{\theta}_3) \times r_{34} + \dots + (n_1 \dot{\theta}_1 + n_2 \dot{\theta}_2 + \dots + n_n \dot{\theta}_n) \times r_{n(n+1)}$$

$$= n_1 \dot{\theta}_1 \times (r_{12} + r_{23} + \dots + r_{n(n+1)}) + n_2 \dot{\theta}_2 \times (r_{23} + \dots + r_{n(n+1)}) + \dots + n_n \dot{\theta}_n \times (r_{n(n+1)})$$

$$= \sum_{k=1}^n n_k \dot{\theta}_k \times r_{k(n+1)}$$

$$\dot{r}_{iE} = \sum_{k=1}^n n_k \dot{\theta}_k r_{k(n+1)}$$

velocity of the end effector

generalize coordinate

could map from θ to ω !

$$\dot{r}_{iE} = \underbrace{[n_1 \times r_{1(n+1)} \quad n_2 \times r_{2(n+1)} \quad \dots \quad n_n \times r_{n(n+1)}]}_{J_{eop}} \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \vdots \\ \dot{\theta}_n \end{pmatrix}$$

$$\omega_{iE} = \sum_{i=1}^n n_i \dot{\theta}_i = \underbrace{[n_1 \quad n_2 \quad \dots \quad n_n]}_{J_{eor}} \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \vdots \\ \dot{\theta}_n \end{pmatrix}$$

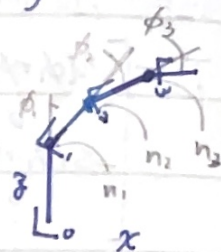
$$I J_{eo} = \begin{bmatrix} J_{eop} \\ J_{eor} \end{bmatrix} = \begin{bmatrix} I n_1 \times r_{1(n+1)} & I n_2 \times r_{2(n+1)} & \dots & I n_n \times r_{n(n+1)} \\ I n_1 & I n_2 & \dots & I n_n \end{bmatrix}$$

$$I n_k = C_{i(k-1)}^{(k-1)} n_k$$

ex. 3-3-2

Determine the Jacobian (geometric) RHS.

$$I J_{eo} = \begin{bmatrix} I n_1 \times r_{1(n+1)} & \dots & I n_n \times r_{n(n+1)} \\ I n_1 & \dots & I n_n \end{bmatrix}$$



$$I J_{op} \in \mathbb{R}^{3 \times 3}$$

$$I J_{or} \in \mathbb{R}^{3 \times 3}$$

$$\left. \begin{aligned} I n_1 &= n_1 = I n_1 = I e_y \\ I n_2 &= C_{11} n_2 = I e_y \\ I n_3 &= C_{12} n_3 = I e_y \end{aligned} \right\} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

$$I r_{iE} = I r_{12} + I r_{23} + I r_{3E}$$

$$= C_{11} r_{12} + C_{12} r_{23} + C_{13} r_{3E}$$

$$= l_1 \begin{pmatrix} \cos \phi_1 \\ 0 \\ \sin \phi_1 \end{pmatrix} + l_2 \begin{pmatrix} \cos(\phi_1 + \phi_2) \\ 0 \\ \sin(\phi_1 + \phi_2) \end{pmatrix} + l_3 \begin{pmatrix} \cos(\phi_1 + \phi_2 + \phi_3) \\ 0 \\ \sin(\phi_1 + \phi_2 + \phi_3) \end{pmatrix}$$

$$I r_{2E} = I r_{23} + I r_{3E}$$

$$= C_{12} r_{23} + C_{13} r_{3E}$$

$$= l_2 \begin{pmatrix} \cos(\phi_1 + \phi_2) \\ 0 \\ \sin(\phi_1 + \phi_2) \end{pmatrix} + l_3 \begin{pmatrix} \cos(\phi_1 + \phi_2 + \phi_3) \\ 0 \\ \sin(\phi_1 + \phi_2 + \phi_3) \end{pmatrix}$$

$$I r_{3E} = I r_{3E}$$

$$= l_3 \begin{pmatrix} \cos(\phi_1 + \phi_2 + \phi_3) \\ 0 \\ \sin(\phi_1 + \phi_2 + \phi_3) \end{pmatrix}$$

assume $l_1 = l_2 = l_3 = l$

$$\therefore I J_{eo} =$$

$$\begin{bmatrix} -l \cos(\phi_1 + \phi_2 + \phi_3) & -l \cos(\phi_1 + \phi_2) & -l \cos(\phi_1 + \phi_2 + \phi_3) & -l \cos(\phi_1 + \phi_2) & -l \cos(\phi_1 + \phi_2 + \phi_3) & -l \cos(\phi_1 + \phi_2) \\ 0 & 0 & 0 & 0 & 0 & 0 \\ l \sin(\phi_1 + \phi_2 + \phi_3) & l \sin(\phi_1 + \phi_2) & l \sin(\phi_1 + \phi_2 + \phi_3) & l \sin(\phi_1 + \phi_2) & l \sin(\phi_1 + \phi_2 + \phi_3) & l \sin(\phi_1 + \phi_2) \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 & 1 & 1 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

ex. 3-3-3

Given

$$r_p = \begin{pmatrix} l_1 C_{11} \dot{\theta}_1 + l_1 C_{12} (\dot{\theta}_1 + \dot{\theta}_2) + l_1 C_{13} (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \\ -l_1 S_{11} \dot{\theta}_1 - l_1 S_{12} (\dot{\theta}_1 + \dot{\theta}_2) - l_1 S_{13} (\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3) \end{pmatrix}$$

$$\omega = \dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3$$

determine Jacobian (geometric)

(cont'd)

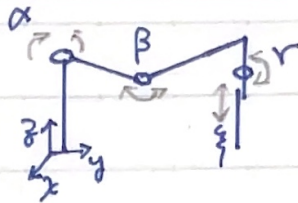
$$W_e = \begin{pmatrix} v_e \\ w_e \end{pmatrix} = J_{e0}(\theta) \dot{\theta}$$

$$\begin{pmatrix} \dot{r}_p \\ \dot{w} \end{pmatrix} = J_{e0}(\theta) \cdot \begin{pmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{pmatrix}$$

$$\therefore J_{e0}(\theta)$$

$$= \begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ -l_1 s_1 & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \end{bmatrix}$$

SCARA Robot Arm



generalized coordinate

$$\vec{p} = [\alpha \ \beta \ \gamma \ \xi]^T$$

geometric rotation Jacobian

$$\varphi = c + \alpha + \beta + \gamma$$

$$\dot{\varphi} = \dot{\alpha} + \dot{\beta} + \dot{\gamma}$$

$$J_{EOR} = [1 \ 1 \ 1 \ 0]$$

geometric position Jacobian

$$\vec{x}_{EP} = \begin{pmatrix} \cos \alpha + \cos(\alpha + \beta) \\ \sin \alpha + \sin(\alpha + \beta) \\ c - \xi \end{pmatrix}$$

$$\dot{\vec{x}}_{EP} = \begin{pmatrix} -\dot{\alpha} \sin \alpha - \dot{(\alpha + \beta)} \sin(\alpha + \beta) \\ \dot{\alpha} \cos \alpha + \dot{(\alpha + \beta)} \cos(\alpha + \beta) \\ -\dot{\xi} \end{pmatrix}$$

$$\therefore J_{EOP} = \begin{bmatrix} -\sin(\alpha) - \sin(\alpha + \beta) & -\sin(\alpha + \beta) & 0 & 0 \\ \cos(\alpha) + \cos(\alpha + \beta) & \cos(\alpha + \beta) & 0 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix}$$

Eigen-decomposition

revison of eigenvalues & eigenvectors

- sets are $\begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} v = w$
- v will hv a span

usually, w is kicked off from the span

some w remains on the span

THIS IS AN EIGENVECTOR

mathematically $Av = \lambda v$

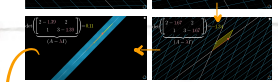
$$Av = \lambda v \Rightarrow (A - \lambda I)v = 0$$

$v \in \text{Null}(A - \lambda I)$ non-trivial subspace

hv to be rank deficient!

$$\det(A - \lambda I) = 0$$

"tweaking λ s.t. $A - \lambda I$ can squeeze



someone to null!"

$$\det \begin{pmatrix} 2 - \lambda & 2 \\ 1 & 3 - \lambda \end{pmatrix} = 0$$

$\Delta \text{Eig}(A) \in \mathbb{C}$ (complex roots)

\Rightarrow hv some rotation!

$$\text{eg. } \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} \rightarrow \pm i$$

Δ double root $\text{Eig}(A)$

\Rightarrow shear

$$\text{eg. } \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$

Δ Eigen-basis \Rightarrow Eigendecomposition

$A \rightarrow$ express w/ new basis w/ eigenvectors

$$A = T^{-1} \Lambda T$$

Δ change of basis

$$\begin{bmatrix} 2 & -1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} a \\ b \end{bmatrix}$$

our grid \rightarrow Jennifer's grid

$$* \begin{bmatrix} A \\ \text{our lang.} \end{bmatrix} \leftarrow \begin{bmatrix} \text{Jennifer's lang.} \end{bmatrix}$$

$$* \begin{bmatrix} A^{-1} T^{-1} A \\ \text{our lang.} \end{bmatrix} \leftarrow \begin{bmatrix} \text{Jennifer's lang.} \end{bmatrix}$$

some transf. that we understand still in our lang.

back to Jennifer!

\rightarrow equivalent transformation in different coordinate!

Eigen-Decomposition (cont'd)

$$\begin{cases} A u_1 = \lambda_1 u_1 \\ A u_2 = \lambda_2 u_2 \end{cases}$$

$$\Rightarrow A \begin{bmatrix} u_1 & u_2 \end{bmatrix} = \begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$$\Rightarrow A U = U \Lambda$$

$$\Rightarrow A = U \Lambda U^{-1}$$

Δ usage 1

rotation

$$\Delta A^n = \Lambda^n$$

$$= U \Lambda^n U^{-1}$$

$$= U \Lambda^n U^{-1}$$

